1	Mechanistic insights into the role of polydopamine					
2	interlayer towards improved separation performance of					
3	polyamide nanofiltration membranes					
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21 ABSTRACT

Interlayered thin-film nanocomposite membranes (TFNi) are an emerging type of 22 membranes with great potential to overcome the permeability-selectivity upper bound 23 24 of conventional thin-film composite (TFC) nanofiltration and reverse osmosis membranes. However, the exact roles of the interlayer and the corresponding 25 26 mechanisms leading to enhanced separation performance of TFNi membranes remain poorly understood. This study reports a polydopamine (PDA) intercalated TFNi 27 28 nanofiltration membrane (PA-PSF2, PDA coating time at 2hr) that possessed nearly an order of magnitude higher water permeance of 14.8 ± 0.4 Lm⁻²h⁻¹bar⁻¹ compared to 29 the control TFC membrane (PA-PFS0) of 2.4 ± 0.5 Lm⁻²h⁻¹bar⁻¹. The TFNi membrane 30 further showed enhanced rejection towards a wide range of inorganic salts and small 31 32 organic molecules (including antibiotics and endocrine disruptors). Detailed 33 mechanistic investigation reveals that the membrane separation performance was enhanced due to both the direct "gutter" effect of the PDA interlayer and its indirect 34 35 effects resulting from enhanced polyamide formation on the PDA-coated substrate, 36 with the "gutter" effect playing a more dominant role. This study provides a mechanistic and comprehensive framework for the future development of TFNi 37 38 membranes.



43 INTRODUCTION

Thin-film composite (TFC) reverse osmosis (RO) and nanofiltration (NF) membranes, 44 consisting of an ultra-thin (~100 nm) polyamide selective layer on an ultrafiltration 45 substrate, are the core for membrane-based desalination and water reuse.^{1, 2} However, 46 47 conventional TFC membranes are strongly constrained by the "upper bound" trade-off between their water permeance and selectivity.³ Recently, a new class of thin-film 48 nanocomposite membranes with an interlayer structure (TFNi) have been reported.⁴⁻⁶ 49 Up to date, a wide range of interfacial coatings have been applied (e.g., 50 polyelectrolytes,⁵ polydopamine (PDA),⁷⁻¹¹ polyphenols,¹² poly(ether ether ketone),¹³ 51 halloysite nanotubes,¹⁴ carbon nanotubes,^{6, 15-17} and their derivatives,^{18, 19}), with some 52 studies showing an order of magnitude higher water permeance and simultaneously 53 enhanced water/solute selectivity for TFNi membranes.^{15, 19, 20} 54

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Despite the great potential of TFNi membranes to overcome the longstanding 56 permeability-selectivity upper bound,³ experimental results often show contradictory 57 58 trends. For example, PDA has been one of the most commonly applied coating materials due to its simplicity, strong adhesion, hydrophilicity, and ease for thickness 59 control.^{21, 22} Many studies have reported PDA as an interlayer coating for the 60 preparation of TFNi membranes.7, 8, 23, 24 While some studies observed enhanced 61 membrane permeance for PDA intercalated membranes,^{8, 10, 18} others reported a slight 62 reduction in permeance.7, 24 Systematic studies are needed to better resolve the 63

64 fundamental mechanisms governing the role of interlayers. In addition, the existing literature on TFNi membranes focuses primarily on salt removal efficiency in the 65 context of desalination.^{7, 10, 23, 25} On the other hand, the removal of trace organic 66 67 contaminants (TrOCs) can be far more important than the removal of simple salts for some important applications such as potable water reuse.^{2, 26} These literature gaps 68 69 prompt us to perform a systematic mechanistic investigation on the fundamental roles 70 of interlayers in membrane formation and in the transport of water, salts, and organic 71 micropollutants through TFNi membranes.

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73 In this study, we use PDA as a model interlayer to investigate its impact on the 74 formation of polyamide NF membranes and their separation performance. We 75 hypothesize that the enhanced water permeance of TFNi membranes is contributed by 76 the combined effects of (1) the shortened transport pathway through the rejection 77 layer upon the inclusion of a highly permeable interlayer (similar to the gutter effect in the context of gas separation²⁷) and (2) the improved formation of the rejection 78 79 layer itself. Polyamide rejection layers were formed on PDA-coated substrates by interfacial polymerization (IP) of piperazine (PIP) and trimesoyl chloride (TMC). We 80 reveal the critical roles of the PDA interlayer on the gutter effect and on the 81 82 physiochemical properties of the polyamide layers, thereby elucidating the governing 83 mechanisms responsible for enhanced water permeance, salt rejection, and TrOCs removal of the TFNi membranes. For the first time, the relative contributions of the 84

direct gutter effect and indirect effect through enhanced membrane formation are
resolved. This study provides critical mechanistic insights to the design and
fabrication of next-generation high-performance NF membranes.

89 MATERIALS AND METHODS

90 Materials and chemicals.

Unless described otherwise, all solutions were prepared from analytical-grade 91 92 chemicals and Millipore ultrapure water. Polysulfone (PSF, Mw. 35,000), N, N-dimethylformamide (DMF, anhydrous 99.8%), piperazine (PIP, ReagentPlus®, 93 99%), trimesoyl chloride (TMC, 98%), and hexane (HPLC grade, 95%) were all 94 purchased from Sigma-Aldrich for the fabrication of PSF substrates and TFC NF 95 membranes. Sodium chloride (NaCl), sodium sulfate anhydrous (Na₂SO₄), 96 97 magnesium chloride (MgCl₂ 6-hydrate), magnesium sulfate (MgSO₄) and calcium chloride anhydrous (CaCl₂) were all purchased from Uni-Chem chemical reagents. 98 D-(+)Glucose (Mw. 180.16, Diekmann), D-Raffinose (Mw 504.44, Macklin) and 99 100 Dextran (Mw 1000 and 2000, D-chem) were used for the evaluation of the pores size 101 of the fabricated TFC membranes. Dopamine hydrochloride (J&K Scientific Ltd., 102 China), tris (hydroxymethyl, Acros Organics, Geel, Belgium) and hydrochloric acid (HCl, 37 wt%, VWR, Dorset, U.K) were obtained for preparing PDA coating. 103 104 Chloroform (VWR, Dorset, U.K) was used as a solvent for isolating polyamide rejection layers. Two endocrine-disrupting compounds (ethylparaben (MW = 166.2 105 Da) and propylparaben (180.2 Da)) and four antibiotics (sulfamethoxazole (253.3 Da), 106 107 sulfamethazine (278.3 Da), norfloxacin (319.3 Da), and ofloxacin (361.4 Da)) were 108 used as model TrOCs, and all these compounds were purchased from Sigma-Aldrich.

109 Synthesis of TFNi membranes.

A PSF substrate was first fabricated by the phase inversion method using a polymer 110 dope of 15 wt% PSF dissolved in DMF following our previous study.¹⁹ PDA coating 111 112 was performed by pouring a 2 g/L dopamine solution containing 10 mM Tris-HCl 113 buffer at pH 8.5 to a membrane coupon placed in a home-made container in such a 114 way that only its front side was exposed to the coating solution over predetermined time duration (1, 2 or 24 hr) under continuous shaking. The PDA-coated PSF 115 116 substrate was denoted as PSFn, where n represents the PDA coating duration (with n 117 = 0 indicating no PDA coating).

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To synthesize the TFNi membrane, an IP reaction was performed on the pristine or 119 120 PDA-modified PSF (Figure 1). Briefly, a 0.2 wt% PIP/H₂O solution was gently poured onto the substrate for 3 min. The excess solution was removed by a rubber 121 122 roller. Then, a 0.15 wt% TMC/hexane solution was introduced to the PIP-impregnated 123 substrate, and the IP reaction was continued for 1 min. Subsequently, the fabricated 124 membrane was rinsed by hexane to remove the unreacted TMC and was further post-treated in an oven for 10 min at 60 °C. The resultant TFNi membrane, denoted as 125 PA-PSFn in accordance to its substrate, was stored in deionized water before further 126 use. In this study, PA-PSF0 stands for the control TFC membrane prepared on the 127 128 pristine PSF substrate without PDA coating.





Figure 1. Schematic diagram on the fabrication of TFC (a) and TFNi membranes (b). To prepare the PDA interlayer, a dopamine solution (2g/L in 10 mM Tris-HCl buffer at pH 8.5) was used to coat the substrate for a predetermined duration (1, 2 or 24 hr). Interfacial polymerization was performed on the substrates with or without PDA coating to obtain TFNi and TFC membranes, respectively. The concentration of PIP was 0.2 wt% and that of TMC was 0.15 wt%.

138 Synthesis of polyamide nanofilms at free aqueous-organic interface.

139 In order to resolve the role of the interlayer on membrane transport properties (e.g., its direct effect as a high-permeability gutter layer²⁷ vs. its indirect effect on the 140 formation of the polyamide layer^{19, 28}), we further synthesized polyamide nanofilms at 141 142 a free interface (PAfi) between an aqueous solution (0.2 wt% PIP/H₂O) and an organic solution (0.15 wt% TMC/hexane).²⁹ Formation of polyamide nanofilms at free 143 interfaces has been well documented in the literature.^{5, 25, 29} The properties of the 144 145 generated polyamide nanofilms depend only on the composition monomer solutions 146 and the reaction time, while the interference of the substrate is prevented. In the current study, the use of identical IP reaction conditions (monomer solutions and 147

reaction time) led to identical polyamide nanofilms. The nanofilms were 148 vacuum-filtrated (filtration time = 1 min) onto the pristine PSF0 substrate and a 149 PDA-coated PSF2 substrate, and the resulting membranes PAfi-PSF0 and PAfi-PSF2 150 151 were then washed by hexane and heat-treated for 10 min at 60°C. In the current study, 152 PAfi-PSF0 and PAfi-PSF2 have identical rejection layers. Therefore, the difference 153 between their transport properties is attributed to the direct effect of interlayer on the substrate. In contrast, the difference between PA-PSF0 and PA-PSF2 can be caused by 154 155 both the direct effect of the substrate and additional indirect effects, noting that the 156 morphology and chemistry of the polyamide layers could be potentially affected by the presence of the interlayer. 157

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159 Membrane characterization.

160 Surface morphology of the membranes and substrates was examined by scanning 161 electron microscope (SEM, LEO 1530, FEG UK) using an accelerating voltage of 5 kV. Prior to the characterization, the membranes samples were coated by platinum and 162 163 gold for 40 seconds. In addition to the front surfaces, the back surfaces of the rejection layers of PA-PSFn membranes were also examined by SEM after dissolving 164 PSF using chloroform following our previous study.¹⁹ Specifically, a piece of 165 166 membrane specimen (0.5 cm \times 0.5 cm) was attached onto a silicon wafer, with its polyamide side facing the silicon wafer. Chloroform, a solvent frequently reported in 167 the literature^{19, 30} for dissolving PSF to isolate the polyamide layer, was applied to 168

rinse the PSF substrate until the white precipitations completely dissappeared from
the sample. According to our previous study,¹⁹ this procedure ensures the complete
removal of the PSF substrate.

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Membrane cross-sectional images were obtained using a transmission electron 173 174 microscope (TEM, Philips CM100, Eindhoven, Netherlands) at an accelerating voltage of 100 kV.³¹ The thickness of the rejection layer was determined from TEM 175 176 micrographs using image software (MediaCybernetics, Inc.). Membrane roughness of 177 the front and back surface of the rejection layers was measured by atomic force 178 microscopy (AFM, Multimode 8, Bruker, MA) with a scanning size of $5 \times 5 \mu m$. The value of root-mean-square roughness (Rq) and maximum roughness (Rmax) was 179 180 obtained using the Nanoscope Analysis software (Bruker, MA). Membrane water 181 contact angle was measured using an automatic contact angle meter (Attension Theta, 182 Biolin Scientific, Sweden) equipped with a video capture device. A membrane 183 specimen was vacuum-dried at room temperature for 24 hr before the measurement. A 184 water droplet of approximately 3 µL was placed on the membrane surface and the contact angle was recorded after a stabilizing time of 10 s. For each membrane type, 185 186 the contact angle measurements were repeated at 10 different locations for two 187 different membrane samples, and the average value was reported. Membrane 188 functional groups and surface elemental compositions were characterized using attenuated total reflection Fourier transform infrared (ATR-FTIR) spectroscopy and 189

190	X-ray photoelectron spectroscopy (XPS), respectively. ³¹⁻³³ A quartz crystal						
191	microbalance with dissipation (QCM-D, E4, Q-Sense Biolin Scientific, Sweden) was						
192	used to quantify the amount of PIP uptake by the control PSF0 and PDA-coated PSF						
193	substrates following our previous study. ¹⁹						

195 Separation performance testing.

Membrane separation performance was tested using a cross-flow filtration setup at 24 °C. A membrane coupon (20.6 cm²) was subjected to an applied pressure of 50 psi (i.e., 3.45 bar) for 1 hr before the measurement of water flux and salt rejection under the same pressure. Additional tests were also included to study the effect of applied pressure on membrane separation performance (see Supporting Information S3). Water flux was determined by weighing the mass of the permeate over a designated time interval:

$$J_{\nu} = \frac{\Delta m}{\Delta t \times A \times \rho} \tag{1}$$

where J_{ν} (L m⁻² h⁻¹) is the water flux, Δm (kg) is the mass of the permeate collected over a duration of Δt (h), A (m²) is the effective membrane area, and ρ (kg L⁻¹) is the density of the permeate water. The membrane water permeance was determined as the ratio of pure water flux over the applied pressure.

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The salt rejection was measured using a feed solution containing a single type of salt
(1000 ppm Na₂SO₄, MgSO₄, MgCl₂, CaCl₂, or NaCl). For each test, a new membrane

coupon was pre-compacted for 1 hr before the collection of permeate samples. The salt rejection *R* was determined based on the conductivity of the feed (C_f) and that of the permeate (C_p) measured by a conductivity meter (Ultrameter II, Myron L company, Carlsbad, CA) using Equation (2). The reported rejection is the average value of three membrane samples from different batches. The separation factor (α) of NaCl to MgSO₄ was calculated based on Equation (3).

$$R = (1 - \frac{C_{\rm p}}{C_{\rm f}}) \times 100\%$$
(2)

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$$\alpha = \frac{(C_{\text{NaCl}} / C_{\text{MgSO}_4})_{\text{p}}}{(C_{\text{NaCl}} / C_{\text{MgSO}_4})_{\text{f}}} = \frac{1 - R_{\text{NaCl}}}{1 - R_{\text{MgSO}_4}}$$
(3)

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220 The propylparaben, sulfamethoxazole, rejection TrOCs (ethylparaben, of 221 sulfamethazine, norfloxacin and ofloxacin) were also evaluated based on our previous work.^{34, 35} Briefly, a feed solution containing a cocktail of TrOCs (200 µg/L for each 222 223 compound) was prepared by introducing 1 mL stock solution of each TrOC (1g/L in methanol) to the feed tank (5 L). An equilibrium time of 12 h was allowed, before 224 feed and permeate samples were collected for further analysis using an 225 ultraperformance liquid chromatograph with double mass spectra (UPLC-MS/MS, 226 Waters ACQUITY).³⁶ According to the literature, the equilibrium time ensures stable 227 228 rejection performance (e.g., by eliminating the potential effect of TrOC sorption by the membrane).³⁶⁻³⁸ The rejection of each TrOC was determined based on the 229 measured feed (C_f) and permeate (C_p) concentrations (Equation (2)) using three 230

231 different membrane samples.

233 **RESULTS AND DISCUSSIONS**

234 **Properties of PSFn substrates.**

Figure 2 presents the properties of the substrates. Compared to the pristine PSF0, the 235 236 PDA-coated substrates became increasingly darker at longer coating time, which is in good agreement with the literature.^{22, 39} The contact angle decreased from $92.6 \pm 5.3^{\circ}$ 237 for PSF0 to $35.3 \pm 2.6^{\circ}$ for PSF24, which can be attributed to the hydrophilic amine 238 and catechol groups of PDA.^{21, 40} The water permeance of the substrate decreased 239 mildly after short-duration coating $(274.5 \pm 35.9 \text{ and } 242.3 \pm 46.8 \text{ Lm}^{-2}\text{h}^{-1}\text{bar}^{-1}$ for 240 PSF1 and PSF2, respectively, compared to $314.8 \pm 14.6 \text{ Lm}^{-2}\text{h}^{-1}\text{bar}^{-1}$ for PSF0). This 241 242 trend is consistent with the decreased substrate pore size after PDA coating (Figure 3a). This decrease in pore size was likely due to the penetration of PDA into substrate 243 pores.^{8, 23} At a coating duration of 24 hr, a large number of PDA aggregates appeared 244 (Figure 3a) - a phenomenon also reported in prior studies.⁷ Although the PSF24 245 246 substrate with the extended coating duration had the lowest water contact angle, its surface pores were extensively covered by PDA, resulting in a dramatically reduced 247 water permeance of $41.3 \pm 9.0 \text{ Lm}^{-2}\text{h}^{-1}\text{bar}^{-1}$ for PSF24. 248



Figure. 2. Contact angle and water permeance of the substrates. Digital photos of the

substrates are also shown.

254 **Properties of PA-PSFn membranes.**

ATR-FTIR results (Supporting Information S1) confirm the formation of polyamide 255 layers after the IP reaction.^{41, 42} Figure 3b-e present the morphological features of the 256 257 PA-PSFn membranes. Both SEM top views (Figure 3b) and TEM cross-sectional views (Figure 3d) show much rougher polyamide surfaces for PA-PSF2 and 258 259 PA-PSF24, which is further confirmed by AFM results (Figure 3e and Table 1). In contrast, the bottom surface of the rejection layers was smoother for the TFNi 260 membranes (PA-PSF1, PA-PSF2, and PA-PSF24) compared to the control PA-PSF0 261 262 (Figure 3c and Table 1). Indeed, the bottom surface of PA-PSF0 had numerous protuberances of several tens to hundreds of nm in size (Figure 3c), which was 263 formed by the intrusion of polyamide into the large-sized pores of its substrate.^{15, 19, 43} 264 265 The much smoother bottom surfaces of the TFNi rejection layers revealed that PDA 266 interlayers were able to prevent such undesirable intrusion of polyamide as a result of reduced pore size for coated substrates.¹⁹ 267

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The apparent thickness of the rejection layer of PA-PSF1 was comparable to that of the control membrane PA-PSF0 (60 - 70 nm, see TEM cross-sections in Figure 3c). In contrast, those of PA-PSF2 and PA-PSF24 were significantly thicker (116 \pm 24 and 201 \pm 37 nm, respectively), which agree well with their much greater surface roughness. Interestingly, the rejection layers of these two membranes contained discrete nanovoids that are not observed for PA-PSF0 and PA-PSF1 (magnified TEM 275 cross-sections images are available in Supporting Information S1). The presence of nanovoids has been frequently reported for fully aromatic polyamide prepared from 276 m-phenylenediamine (MPD) and TMC.^{30, 44, 45} Our prior studies suggest that CO₂ 277 278 dissolved in the high-pH aqueous amine solution plays a critical role in forming such 279 nanovoids: (1) the acid and heat produced during the IP reaction cause the interfacial degassing of CO₂ nanobubbles (HCO₃⁻ + H⁺ $\xrightarrow{\Delta}$ CO₂↑ + H₂O);^{46, 47} (2) these 280 281 nanobubbles are retained between the substrate and the polyamide layer, resulting in the formation of nanovoids accompanied with increased surface roughness.⁴⁶⁻⁴⁸ 282 283 Although such nanovoids are less frequently observed for semi-aromatic polyamide prepared from PIP and TMC due to the slower reaction and less reaction heat 284 generated,⁴⁶ the current study show the feasibility to enhance nanovoid formation by 285 286 introducing an interlayer. This enhanced nanovoid formation is likely due to the 287 combined effects of (1) greater PIP sorption at longer PDA coating duration (Figure 4a) and thus greater interfacial heating effect;^{29, 49} and (2) the improved gas 288 confinement as a result of smaller surface pore size of the PDA-coated substrates.^{28, 48} 289 290 The presence of nanovoids in PA-PSF2 and PA-PSF24 partially explains their greater surface roughness, although that of PA-PSF24 could also be affected by the rough 291 292 surface of its substrate (Figure 3a). According to the literature, these nanovoids are 293 beneficial to provide thinner intrinsic polyamide thickness (i.e., the true thickness 294 excluding nanovoids), increased effective filtration area, and enhanced water transport pathways.^{44, 45, 50, 51} In current study, the contact angle (Table 1) was not significantly 295



Figure 3. Microscopic characterization of PSFn substrates and PA-PSFn membranes: (a) SEM
micrographs of substrate surfaces; (b) SEM micrographs of the top surfaces of PA-PSFn; (c)
SEM micrographs of the bottom surfaces of the rejection layers isolated from PA-PSFn; (d)
TEM micrographs of the cross-sections of PA-PSFn; and (e) AFM micrographs of the surface
morphology of PA-PSFn. The scale bar for SEM is 500 nm and the scale bar for TEM is 100
nm.

Top surface of rejection layer			Bottom surface of rejection		Contact angle of
	Top surface of rejection layer		layer		membrane top surface
	<i>R</i> q (nm)	Rmax (nm)	Rq (nm)	Rmax (nm)	(°)
PA-PSF0	18.4 ± 1.5	150.7 ± 10.4	44.2 ± 8.9	244.7 ± 19.1	53 ± 4
PA-PSF1	30.8 ± 2.4	221.0 ± 20.2	13.7 ± 2.6	111.1 ± 18.1	55 ± 4
PA-PSF2	36.2 ± 1.1	283.3 ± 14.7	18.3 ± 2.7	122.8 ± 12.8	54 ± 2
PA-PSF24	32.6 ± 0.8	318.7 ± 18.2	20.3 ± 1.4	134.3 ± 17.3	49 ± 2

Table 1. Roughness and water contact angle results of the PA-PSF membranes.

308 Figure 4b presents the O:N ratio and crosslinking degree, both calculated from the XPS results (Supporting Information S1). The O:N ratio of the PA-PSF1 (1.28 ± 0.03) 309 was significantly lower than that of the control PA-PSF0 membrane (1.50 ± 0.07), 310 revealing an enhanced crosslinking degree³⁴ with the introduction of the PDA 311 interlayer (63.3 \pm 3.7% for PA-PSF1 vs. 41.0 \pm 5.2% for PA-PSF0). At longer PDA 312 313 coating duration, the crosslinking degree was further improved. This result can be 314 well explained by the enhanced PIP sorption by the PDA-coated substrates (Figure 315 4a), with a greater effective PIP concentration in the IP reaction leading to a more crosslinked polyamide.⁷ Consistent with the XPS-based crosslinking analysis, pore 316 317 size analysis based on the rejection of neutral solutes (Figure 4c and Supporting 318 Information S2) shows that the TFNi membranes with PDA-coated substrates had significantly smaller effective mean pore sizes ($\mu_p \sim 0.34$ -0.36 nm) compared to that 319 320 of the control PA-PSF0 membrane ($\mu_p \sim 0.51$ nm).



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Figure 4. Membrane characterization by QCM-D, XPS and pore size analysis. (a) QCM-D measurements of PIP sorption (0.2 wt% PIP aqueous solution) onto quartz sensors coated with PSF or PDA-modified PSF following our previous study;¹⁹ (b) oxygen/nitrogen ratio ($r_{O/N}$) based XPS results (see Supporting Information S1) and the corresponding crosslinking degree calculated by $(4-2r_{O/N})/(1+r_{O/N})$;³⁴ and (c) pore size distribution and effective mean pore radius (μ_p) of PA-PSF membranes based on rejection results of glucose, raffinose, and dextran (Mw = 1k and 2k). See detailed calculations in Supporting Information S2.

331 Membrane separation properties.

Among the four PA-PSF membranes prepared in the current study, PA-PSF1 had the 332 highest water permeance of 19.3 ± 0.8 Lm⁻²h⁻¹bar⁻¹, showing an approximately one 333 334 order of magnitude improvement over that of the control PA-PSF0 membrane (2.4 \pm 0.5 Lm⁻²h⁻¹bar⁻¹, Figure 5a). Further increasing in PDA coating duration decreased the 335 membrane water permeance to 14.8 ± 0.4 Lm⁻²h⁻¹bar⁻¹ for PA-PSF2 and 10.7 ± 1.5 336 Lm⁻²h⁻¹bar⁻¹ for the PA-PSF24, possibly as a result of greater hydraulic resistance of 337 the PDA coating. Nevertheless, the permeance values of both PA-PSF2 and PA-PSF24 338 339 were substantially greater than that of the control PA-PSF0 membrane without the PDA interlayer. This dramatic enhancement of TFNi membranes over their TFC 340 control can be attributed to (1) the direct role of PDA interlayer as a high-permeability 341 gutter layer to optimize the water transport pathway,⁵²⁻⁵⁴ and (2) its indirect effect 342 343 through the influence of the interlayer on polyamide formation (e.g., elimination of polyamide intrusion, formation of nanovoids, and increased membrane surface 344 roughness (Figure 3)). 345

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The PDA intercalated TFNi membranes had significantly enhanced rejection of Na₂SO₄, MgSO₄, MgCl₂, and CaCl₂ over that of the TFC control though the effect on NaCl was less obvious (Figure 5b). The greatly improved removal efficiency was primarily due to the formation of a more crosslinked polyamide rejection layer (Figure 4c). Nevertheless, the membrane PA-PSF24 membrane with the longest PDA 352 coating time had comparable salt rejection with PA-PSF2, even though the former had a higher crosslinking degree. This observation can be explained by the significantly 353 lower water permeance of PA-PSF24, noting that the permeate solute concentration is 354 given by the ratio of solute flux over the water flux.³ Although the excessive PDA 355 356 coating time of 24 h can cause an increase in crosslinking degree and thus reduce the 357 solute flux through the membrane, the simultaneous decrease in water flux reduces its effectiveness in improving the permeate water quality. Our results reveal the critical 358 importance of the coating time (and thus the thickness of the interlayer) to achieve 359 360 optimized membrane separation performance.

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The monovalent over divalent ion selectivity (e.g., $\alpha_{NaCl/MgSO4}$) is of great practical 362 363 interest for NF applications to allow the retaining of divalent ions without the need to pay for the osmotic pressure penalty of NaCl.¹⁹ In this study, PA-PSF2 had the highest 364 365 $\alpha_{\text{NaCl/MgSO4}}$ value of 34.4 ± 1.0, far exceeding those of the control membrane PA-PSF0 and the commercial membranes NF270 and NF90. Figure 5c presents an upper bound 366 367 correlation between water permeance A and $\alpha_{NaCl/MgSO4}$ for conventional TFC membranes prepared by PIP/TMC chemistry.¹⁹ The PA-PSF1 and PA-PSF2 prepared 368 in this study, along with a number of other TFNi membranes reported in the recent 369 alcohol,⁴¹ 370 years based on polyvinyl cellulose nanocrystals,55 (e.g., metal-organic-frameworks,⁵⁶ carbon nanotubes^{6, 15} and tannic acid/Fe³⁺ complexes¹⁹) 371 successfully surpass this upper bound, revealing the huge potential of such an 372





376 Figure 5. Membrane separation performance. (a) Pure water permeance and NaCl to MgSO₄ 377 selectivity. Membranes NF270 and NF90 were included as commercially available benchmarks. (b) Salt rejection of Na₂SO₄, MgSO₄, MgCl₂, CaCl₂ and NaCl. Each rejection 378 379 was measured using a 1000 ppm solution containing a single type of salt. The applied 380 pressure was 50 psi and the temperature of the feed solution was approximately 24 °C. (c) 381 Comparison the separation performance of TFNi membranes with the upper bound tradeoff 382 for conventional TFC membranes. This trade-off between pure water permeance and NaCl/MgSO₄ selectivity was modified from Ref.¹⁹ with copyright permission. The square 383 symbols represent TFNi membranes published in recent literature.^{6, 19, 41, 55, 56} 384

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386 Mechanistic investigation of PDA interlayer.

387 To resolve the exact roles of the PDA interlayer on the separation properties of the 388 resulting TFNi membranes, additional polyamide films were synthesized at a 389 support-free interface between an aqueous PIP solution and a TMC/hexane solution and were transferred onto PSF0 or PSF2. Therefore, the resulting membranes
PAfi-PSF0 and PAfi-PSF2 had identical polyamide rejection layers but different
substrates (without or with a PDA interlayer). In contrast, their counterparts PA-PSF0
and PA-PSF2 (prepared directly on substrates) not only had different support
structures but also different polyamide structures (Figure 3 and Figure 4).

396 Figure 6a,b presents the water permeance and salt rejection of these four membranes. 397 PA-PSF0 and PAfi-PSF0, both had identical recipes for the IP reaction and identical 398 substrate (PSF0), show comparable water permeance of approximately 2.5 399 Lm⁻²h⁻¹bar⁻¹. The corresponding TFNi membranes with a 2-h PDA coating (PA-PSF2 400 and PAfi-PSF2) both had dramatically enhanced water permeance. For example, the 401 permeance enhancement factor of PA-PSF2 ($f_{PA-PSF2}$ = permeance of PA-PSF2 ÷ 402 permeance of the control PA-PSF0 - 1), was 6.13. As discussed in the section 403 "Membrane separation properties", this enhancement in permeance can be attributed to the improved properties of the PDA-coated substrate (f_{sub}) and/or the improved 404 405 properties of the rejection layer (f_{rej}) . In comparison, the permeance enhancement factor of PAfi-PSF2 (f_{PAfi-PSF2}) was 4.73, which is solely attributed to the enhanced 406 substrate (f_{sub}) for which the PDA layer serves as a high permeability gutter layer. 407 408 Although the concept of gutter layer is less discussed in the context of water filtration 409 membranes, this concept has been well established for gas separation membranes to achieve enhanced permeance.52-54, 57 A recent modeling paper27 shows that the 410

411 inclusion of a high-permeability gutter layer allows gas molecules to take a much 412 shorter transport path in the rejection layer, which would also be applicable to TFNi membranes (Figure 6c). In the current study, the difference between $f_{PA-PSF2}$ and 413 414 $f_{PAfi-PSF2}$ can be attributed to the indirect effect of the substrate on the formation of polyamide rejection layer ($f_{rej} = 1.40$). According to recent studies, the substrate 415 serves the important roles as a reservoir for amine monomers^{19, 28} and for providing 416 confinements to the interfacially degassed nanobubbles.^{28, 48} In this respect, the 417 interlayer can (1) simultaneously enhance the amine monomer uptake (Figure 4a) and 418 the confinement effect (due to reduced substrate pore size¹⁷) to result in a rougher and 419 nanovoid-containing polyamide rejection layer (Figure 3d) and (2) also eliminate its 420 intrusion into the substrate (Figure 3c and Ref.¹⁹), both leading to improved water 421 422 transport. Nevertheless, the current study reveals that this indirect effect on rejection layer ($f_{rej} = 1.40$) was much weaker compared to the direct "gutter layer" effect of the 423 substrate ($f_{sub} = 4.73$), possibly due to the weaker ability of the PIP/TMC chemistry 424 for interfacial degassing.⁴⁶ 425

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Figure 6b shows the membrane salt rejection. PA-PSF2, PAfi-PSF0, and PAfi-PSF2 had comparable Na₂SO₄ and NaCl rejection values, which were significantly better than the respective values of PA-PSF0. The poorer rejection performance of PA-PSF0 is consistent with its lower crosslinking degree (Figure 6c), possibly caused by the limited availability of PIP in the PSF0 substrate.²⁸ In contrast, polyamide prepared on

PDA coatings (PA-PSF2) or at free interfaces (PAfi-PSF0 and PAfi-PSF2) enjoy a
greater supply of PIP (e.g., see Figure 4a for PA-PSF2). In addition, previous studies^{19,}
^{28, 58} have demonstrated the greater propensity of defect formation for polyamide
rejection layers prepared over relatively large substrate pores.



Figure 6. Mechanistic insights on the role of the interlayer. The upper panel presents (a) pure water permeance and (b) Na₂SO₄ and NaCl rejection of membranes prepared directly on the substrate (PA-PSF0 and PA-PSF2) and those prepared at a free interface (PAfi-PSF0 and PAfi-PSF2). Membrane performance was tested at an applied pressure of 50 psi at 24 °C. The lower panel presents a schematic illustration (c) of the mechanisms leading to improved



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Figure 7. Membrane rejection results of the control PA-PSF0 and PA-PSF2 membrane on neutral solutes (glucose, raffinose and dextran) and TrOCs (sulfamethoxazole, sulfamethazine, norfloxacin, ofloxacin, ethylparaben and propylparaben). The rejection tests for neutral solutes (glucose, raffinose and dextran) was measured using a 200 ppm solution containing a single type of solute. For TrOCs, the rejection tests were measured using a solution containing a cocktail of six compounds (200 ppb for each TrOC). The applied pressure was 50 psi and the temperature of the feed solution was approximately 24 °C.

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454 IMPLICATIONS AND FUTURE PERSPECTIVES

In this study, we fabricated a PDA-intercalated TFNi NF membrane. The PDA interlayer serves as a highly permeable gutter layer for optimized water transport pathways (Figure 6c). At the same time, this interlayer prevents the intrusion of polyamide into the substrate pores, promotes the formation of nanovoids within the polyamide rejection layer, and increases its crosslinking. The direct "gutter" effect of

the PDA interlayer together with its indirect effects resulting from enhanced 460 polyamide layer led to an order of magnitude higher water permeance along with 461 improved solute rejection for the PDA-intercalated TFNi membrane. We further 462 463 reveal that the direct "gutter" effect played a more dominant role compared to the 464 indirect effects through systematic comparison of PA-PSFn membranes with their 465 counterparts synthesized at a free interface. Future studies should further investigate the separate optimization of the "gutter" effect of the interlayer (with due 466 considerations to its permeability and geometry²⁷) and the indirect effects (via its roles 467 468 as reservoir for monomers and confinement to interfacially degassed nanobubbles²⁸). These effects should also be further validated for the wide range of other interlayer 469 materials such as CNTs,^{6, 15} polyphenols,^{12, 19} and etc.^{5, 56} 470

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472 Existing literature on NF membrane synthesis often emphasize water permeance and 473 salt rejection. Many practical applications, however, requires high selectivity more than high permeance,59,60 particularly for the removal of TrOCs in the context of 474 water reuse.^{2, 36} The PA-PSF2 developed in this study was further tested for its 475 removal efficiency against a set of neutral hydrophilic solutes (glucose, raffinose and 476 dextran) and TrOCs (sulfamethoxazole, sulfamethazine, norfloxacin, ofloxacin, 477 478 ethylparaben and propylparaben). Compared to the control TFC membrane, the PDA-intercalated TFNi membrane shows consistently improved removal of all 479 compounds, thanks to the increased crosslinking degree (Figure 4c) and smaller 480

effective membrane pore size (Figure 4d). Indeed, the multilayered structure itself offers additional opportunities for enhanced removal of TrOCs,^{35, 36, 61} with the possibility to design the interlayer for widened removal spectrum and better efficiency.⁶² The current study reveals the feasibility to simultaneously enhance water permeance, salt rejection, and removal of TrOCs. Future studies on systematic modelling and experimental optimization are needed to fully unleash the potential of TFNi membranes for various environmental applications.

488

489 ASSOCIATED CONTENT

490 The Supporting Information is available free of charge on the ACS Publications491 website at DOI:

492 S1. ATR-FTIR, magnified TEM images and XPS spectra of PA-PSF membranes;

- 493 S2. Methods of determining pore size distribution; S3. Effect of pressure on
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- 501 Notes
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