

1 **An experimental investigation of the roles of water content and gas decompression rate for**  
2 **outburst in coal briquettes**

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7 **Abstract:** The coal and gas outburst has become a worldwide challenge and is still not fully  
8 understood. In this study, an experimental investigation was carried out for outburst evolution.  
9 Coal briquettes were fabricated based on less than 0.6 mm pulverized coal particles of Tunliu  
10 Coal Mine. CO<sub>2</sub> was used to simulate outbursts by saturating coal briquettes in varying gas  
11 pressures (0.2, 0.4 and 0.6 MPa). The outbursts of coal briquettes were induced when rapid gas  
12 decompression was performed. The results indicate the outbursts depend on the gas pressure,  
13 water content and the rate of gas decompression. The differential pressure between the gas inside  
14 and outside the coal briquette is essential to outbursts and varies for different **water contents**  
15 while other parameters affect the initiation and intensity of outbursts as well. The higher gas  
16 pressure the more intense outburst occurs. It is worth noting that low rate of gas decompression  
17 cannot activate any outburst in the experiments even for a high gas pressure. The water content  
18 affects the outburst strongly. The critical minimum gas pressure in the coal briquettes with high  
19 water content becomes much higher than that in the coal briquettes with low water content. The  
20 major energy of the outbursts in the experiments is the expansion energy of the free state gas  
21 inside the coal briquettes. This study clearly demonstrates the progressive fragmentation of  
22 outbursts due to gas decompression.

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25

## 26 **1 Introduction**

27 Coal and gas outbursts are well known as the sudden and violent energy release of coal and  
28 gas that results from a comprehensive function of gas pressure, in-situ stress, coal strength, etc.

29 The first coal and gas outburst accident was reported in France in 1843 and led to two fatalities.

30 Since then, over 30,000 coal and gas outbursts occurred in China, Russia, Poland, Turkey, etc. [1,

31 2]. For instance, on 20<sup>th</sup> October 2004, Daping coal mine in Henan Province, China, occurred a

32 methane explosion due to a coal and gas outburst, resulted in 148 deaths (Xinhuanet). Moreover,

33 as mining depth increases, underground mining and tunnelling have to face more severe

34 situations, especially in terms of outbursts when gases are involved.

35 Coal is a porous material containing various pores and voids, thus these pores and voids can

36 be filled with gases during their formation at depth, e.g. methane (CH<sub>4</sub>) and carbon dioxide

37 (CO<sub>2</sub>). As investigated, there is a large number of gases storing inside the coal seam. The gas can

38 have high pressure after formation at depth. The gases with pressure occupies the microvoids of

39 coal and can result in instantaneous coal and gas outburst accidents. The gases inside coal are not

40 only free state in coal but mostly adsorbed on pore surface [3]. The adsorbed gas typically

41 accounts for 98% of total stored gas in the coal seam, which varies with the adsorbed pressure

42 [4]. The adsorbed state gas has the potential becoming free state gas as gas pressure, temperature

43 or in-situ stress change. The free and adsorbed gases can result in alterations of physical (e.g.

44 swelling) and mechanical behaviours (e.g. strength) [5-8]. High-pressure gases of coal induce

45 severe consequences and high outburst proneness. In particular, an outburst has been recognised

46 that gas pressure is one of the key factors. When the gases run out, an outburst could be less  
47 likely to occur. The gases with pressure will escape because of gas pressure gradient and release  
48 expansion energy. Therefore, the role of gas acting on outbursts is rather significant for the  
49 mechanism of outbursts, however, there is still no clear understanding of the effects of gas  
50 during the process of outburst, which is briefed below.

51 The mechanism of outbursts has been studied since outburst occurred [9-11]. Though the  
52 proposed mechanisms can address some aspects of the outburst process, there is still a lack of  
53 full and clear understanding of the complete process. In the early 1950s, the extensive efforts  
54 have been made [12-14] with consideration of the mechanisms of sorption/desorption of gas and  
55 stress in the generation of outbursts. Outbursts involve many factors, e.g. gas pressure, physical  
56 and mechanical of coal. Some authors have also considered outbursts as gas-involved rockbursts  
57 which are another severe hazard in underground mining and tunnelling [15, 16]. Experimental  
58 studies on outbursts have been conducted [17-19] which involved the factors of gas pressure, in-  
59 situ stress, and coal strength. As involved with a large number of gases, more violent and wide  
60 damage will take place in the accidents. Undoubtedly, the gases with pressure must play a key  
61 factor for the severe results. Only a few studies have experimentally conducted on the how the  
62 gas acts on outbursts [20-22]. It has been shown that outbursts are a gas-driven explosive  
63 eruption phenomenally and gases alone can lead to a violent eruption. Valliappan and Wohua [23]  
64 analysed the gas energy during outbursts and found that both free gas and desorbed gas  
65 contribute to outbursts, and the major energy is from the desorbed gas in the coal. An  
66 experimental study on the energy release from Yang et al. [24] indicates the first 10 seconds of  
67 gas release is significant to the occurrence of outbursts. The role of gas expansion energy during  
68 the outburst is still remained to be understood. Therefore, a better understanding of the

69 mechanism of outbursts is urgently required to resolve the serious consequences of outbursts [1,  
70 9, 11, 25].

71 The present work concentrates on the experimental simulation of outbursts considering gas  
72 pressure, the rate of gas decompression, and water content. This study aims to study the  
73 evolution of outbursts and how the internal gas of coal acts on outbursts based on a  
74 comprehensive experimental investigation. The energy components that contribute to the  
75 outburst were analysed and compared.

## 76 **2 Experimental**

### 77 **2.1 Experimental apparatus**

78 An experimental apparatus was designed to investigate the effects of high pressure gas on  
79 outburst phenomenon. It mainly consists of a compression test machine, a transparent acrylic cell,  
80 two end plates and a gas tank. The experimental apparatus is similar to that in Guan et al. [22],  
81 which have been validated for simulating coal outburst with CO<sub>2</sub> and implying magma  
82 fragmentation of volcanoes. The overview of the experimental apparatus is illustrated in Fig. 1.  
83 The cell has an inner diameter of 120 mm and a height of 330 mm. There are two outlets in the  
84 bottom plate. One is for injecting gas and the other one is for recording the pressure of the gas in  
85 the cell. The gas is supplied by a gas tank and its pressure is controlled by a regulator.

86 In the experiments, CO<sub>2</sub> is used in the experiments instead of CH<sub>4</sub>. One reason is that CO<sub>2</sub> has  
87 no chemical explosion such that it is much safer than CH<sub>4</sub>. Another reason is that the adsorption  
88 capacity of CO<sub>2</sub> is larger than CH<sub>4</sub> in coal for pure gases [26]. Thus, CO<sub>2</sub> has the ability to cause  
89 outbursts easier than CH<sub>4</sub>. There could be more violent and severe consequences of outbursts if  
90 CO<sub>2</sub> is involved. It is significant to use CO<sub>2</sub> for outburst mechanism investigation.

## 91 2.2 Sample preparation

92 Our experimental setup is designed based on the triaxial test setup in soil mechanics. The  
93 transparent cell has the pressure limitation of 1.0 MPa. The regulator of the CO<sub>2</sub> tank can provide  
94 only ~ 1.2 MPa for the experiments. However, based on the test results of the raw coal, the raw  
95 coal samples have much higher UCS (12.14 MPa) and tensile strength (1.05 MPa) than the  
96 briquette samples. Accordingly, the experimental setups must resist higher pressure of saturated  
97 gas for longer time which depends on the permeability and adsorption capacity. Moreover, the  
98 laboratory safety is also considered, a new setup cannot be used before safety evaluation.  
99 Consequently, the briquettes were used instead of raw coals in the experiments. The briquettes  
100 are made of pulverized coal, and they can have similar properties to those weak raw coals.  
101 Previous studies also indicated that coal briquettes possess similar properties to a physically  
102 altered coal such as mylonite, which can be found near the “outburst zones” [27]. They can be a  
103 representative of the coal and be used to investigate outbursts. In this study, the coal samples are  
104 collected from Tunliu Coal Mine in Taiyuan, China. According to the coal proximate analysis of  
105 the coal, the used coal is a high-rank coal and has volatile matter content  $V_{daf}$  of 11.8 %. After  
106 being pulverized, less than 0.6 mm coal particles and employed to fabricate coal briquettes. The  
107 capability of CO<sub>2</sub> adsorption/desorption of the pulverized coal particles can be referred to the  
108 tests of Li et al. [28].

109 The coal briquettes are made of pulverized coal particles and water under compaction. Excess  
110 water will be expelled due to compaction. The compaction of about 20 MPa is held for 1 hour.  
111 Although excess water is expelled during the compaction, the fresh coal briquettes still have high  
112 water content. Fresh coal briquettes can become dry coal briquettes after 2-day air-drying.

113 The uniaxial compressive strengths (UCS) of the two coal briquettes are notably different. The  
114 fresh coal briquette with high water content (14.82 %) has a higher UCS than the dry coal  
115 briquette with low water content (1.09 %), i.e. 0.36 MPa vs. 0.22 MPa. In terms of failure strain,  
116 the high water content coal briquette (2.26 %) presents higher than the low water content coal  
117 briquette (1.97 %). Therefore, the coal briquette with high water content indicates ductile failure  
118 while the coal briquette with low water content shows brittle failure. Slight larger Young's  
119 modulus is found by comparing with the two stress-strain curves, i.e. 19.50 MPa vs. 13.38 MPa.  
120 Brazilian disc tests were also performed to determine the tensile strength of the coal briquettes  
121 based on the suggested methods of the ISRM [29, 30]. The tensile strengths are 0.018 and 0.012  
122 MPa for the high water content and low water content coal briquettes respectively.

### 123 **2.3 Experimental procedure**

124 Prior to injecting CO<sub>2</sub> into the cell, a coal briquette is placed into the cell and the two end  
125 plates are fixed to make sure the plates and cell are sealed well. By adjusting the compression  
126 machine such that the plates are pressurised to a specified load, e.g. 0.5~1.0 MPa, to prevent high  
127 pressure gas escaping from the cell during the experiments. Because of the low permeability of  
128 coal samples, the penetration of the gas is slow. A specified saturation duration for gas  
129 penetration and adsorption is determined. As a result, the adsorbed pressure of the gas reaches  
130 the same value of the pressure of the saturated gas. The saturation duration of CO<sub>2</sub> is estimated  
131 from  $t = r^2/D$  where  $t$  is time,  $r$  is the radius of coal specimens, and  $D$  is CO<sub>2</sub> diffusivity of  
132 coal [31]. For the fabricated coal briquettes, their diffusivity is larger than that of raw coal.  
133 Therefore, a sufficient saturated duration is kept at 10 hours in the experiments. In the saturation  
134 process, the CO<sub>2</sub> tank continually supplies gas to keep the saturated pressure be constant. The

135 gas detector is set to 0 for the atmospheric pressure. Thus the value of the gas detector is the  
136 differential pressure between inside and outside gas.

137 Thereafter, decompression of saturated gas is performed after a coal briquette completes CO<sub>2</sub>  
138 infiltration and adsorption. The pressure of saturated gas drops down and approaches to the  
139 atmospheric pressure. But the gas inside the coal briquette cannot run out during the outside gas  
140 decompression, and then the differential pressure between inside and outside gas is formed. The  
141 differential pressure results in the gas expansion potential and generating tension against coal  
142 briquettes. During the gas decompression, the gas pressure in the cell is measured to figure out  
143 the process of gas acting on outburst.

### 144 **3 Results and discussion**

#### 145 **3.1 Experimental observation**

146 Typical nine coal briquettes were performed to investigate the mechanism of outburst. Table 1  
147 presents the parameters of coal briquettes in the experiments. Not all coal briquettes occurred  
148 outburst due to insufficient conditions. As concluded, there are three different phenomena  
149 occurring in the coal briquettes: Case 1: coal briquettes were still intact after gas decompression;  
150 Case 2: obvious fractures were found in the coal briquettes; Case 3: so-called outbursts occurred.

151 Case 1 (Intact coal briquettes) means only degassing occurred and the adsorbed gas and free  
152 gas diffused towards the outside. The internal gas pressure is lower than the critical pressure such  
153 that no damage happened in the coal. Case 2 (The fractures of coal briquettes) results from the  
154 propagation of cracks and fissures due to the internal gas. However, the growth of fractures  
155 depends on the various parameters, e.g. gas pressure and the strength of coal briquettes. Fracture  
156 growth stops if the gas pressure and contents are insufficient. Finally, fractures but no  
157 fragmentation occur in coal briquettes. Fig. 2(a)-(c) shows the fracture results of coal briquettes

158 after gas decompression under varying gas pressures. When the saturated gas pressure is 0.2 MPa,  
159 only a few and small fractures were found in the coal briquette. For 0.4 MPa saturated gas, there  
160 were more and larger fractures in the coal briquette. As improved to 0.6 MPa of saturated gas,  
161 more fractures were found in the coal briquette. Furthermore, small fragments were separated  
162 from the main body of the coal briquette. This observation indicates the outburst occurs in the  
163 coal briquette when the saturated gas pressure exceeds 0.6 MPa after rapid gas decompression  
164 (Case 3).

165 Compared with the coal briquettes with high water contents, low water content coal briquettes  
166 are liable to occur outburst (Case 3). The outburst fragments in Fig. 2(d)-(f) demonstrate the  
167 outburst phenomena of coal briquettes after gas decompression. Intact coal briquettes became  
168 fragments due to growth and coalescence of the gas induced fractures. It is observed that the  
169 fragment size decreased as gas pressure increased. The saturated pressure of CO<sub>2</sub> of 0.2 MPa  
170 resulted in a slight degree of fragmentation while considerable fragmentation was found if the  
171 CO<sub>2</sub> pressure increased to 0.4 and 0.6 MPa.

172 In terms of the process of the outburst, the outburst only takes several microseconds, see Fig. 3.  
173 Fracture initiation takes place in the microstructure of coal briquettes. It depends on the growth  
174 velocity of cracks which is relied on gas pressure and contents. Once the fracture coalescence  
175 completes, fragmentation is formed such that undissipated free gas and desorbed gas act on these  
176 fragments. As a result, the fragments will be ejected at a specific velocity resulted from the  
177 pressure and content of the gas.

### 178 **3.2 Intensity of outbursts**

179 As experimental results show, the intensity of outburst depends on gas pressure, gas  
180 decompression rate and water content of coal briquettes. To describe the intensity of coal and gas



181 outburst, the degree of fragmentation is introduced. The degree of fragmentation is defined as the  
182 mass ratio of the residual fragment to total mass [22]. Therefore, the normalised intensity of  
183 outburst  $f$  is calculated by the following equation and shown in Table 1:

$$f = \frac{m_t - m_r}{m_t} \times 100\% \quad (1)$$

184 where  $m_t$  and  $m_r$  are the total mass and the largest fragment of coal briquettes after outbursts.

### 185 **3.3 Effect of gas pressure on outbursts**

186 The main energy of outbursts comes from the release of gas. It is obviously known that  
187 outbursts must occur only when gas pressure reaches a threshold. The critical gas pressure is  
188 significant to evaluate the risk in underground mining engineering. The outbursts have been  
189 experimentally studied in terms of high pressure gas [20, 22]. Critical values of gas pressure  
190 have been realised for outburst-prone assessment [32], they are 0.15, 0.74 and 1.00 MPa in  
191 Czech, China and Russian respectively. It indicates that outbursts can occur even for low-  
192 pressure gases of coal.

193 According to the results shown in Figs. 4-5, an outburst will not occur until a critical gas  
194 pressure is reached. The critical gas pressure of coal briquettes for outbursts could be lower than  
195 0.2 MPa since the strength of the coal briquettes is low. The normalised outburst intensity  
196 increases dramatically as gas pressure increases. At the gas pressure of 0.4 MPa, the normalised  
197 intensity  $f$  is improved to 67 %. A normalised intensity of outburst of 89 % arrives when the gas  
198 pressure reaches 0.6 MPa. In contrast, the higher gas pressure is required to generate outburst of  
199 the coal briquettes with higher strength.

### 200 **3.4 Effect of water content of coal briquettes on outbursts**

201 In the experiments, two different coal briquettes showed different critical gas pressures  
202 accordingly. The coal briquettes with high water content and high strength (average water

203 content of 14.08 % and UCS of 0.36 MPa) were difficult to occur outbursts until the high gas  
204 pressure of 0.6 MPa was reached. In comparison, the critical gas pressure decreased to 0.2 MPa  
205 in terms of the coal briquettes with low water contents and low strength (average water content  
206 of 1.09 % and UCS of 0.22 MPa), as shown in Fig. 4(a). The higher water content of coal  
207 briquettes corresponds to the weaker intensity of outbursts. Water occupies the micropores and  
208 voids of the coal and prevention of gas flow, which results in the reduction of gas in the coal.  
209 The effective permeability of gas in coal will decrease as the increase of water content [33]. Less  
210 gas is involved in the outburst process, consequently, the intensity of coal can be weakened. The  
211 experimental result agrees with the analysis of prior studies [17, 34] and field observation [35].

### 212 **3.5 Effect of rate of gas decompression on outbursts**

213 In our experiments, the rate of gas decompression is indicated as a key factor to induce  
214 outbursts. Since the limitation of the experimental apparatus, the rate of gas decompression is  
215 difficult to be controlled continuously. Only two different rates of gas decompression were  
216 conducted in the experiments, e.g. 0.60 and 6.23 MPa/s. Coal briquettes were employed in the  
217 outburst experiments. According to the results, the rate of gas decompression affects the outburst  
218 of coal briquettes, see Fig. 4(b). For the high rate of gas decompression, 6.23 MPa/s, outbursts  
219 occurred at the gas pressure of 0.2 MPa. However, under the low rate of gas decompression of  
220 0.60 MPa/s, there was no outburst occurring even the gas pressure was increased to 0.60 MPa.  
221 Therefore, a critical rate of gas decompression is essential to the occurrence of outbursts in the  
222 experiments. The rate of gas decompression can correspond to the permeability and emission of  
223 gas in the coal seam.

## 224 3.6 Evolution of outbursts

### 225 3.6.1 Gas adsorption/desorption process from coal

226 The gas in the micropores of coal are divided into free state gas and adsorbed state gas [3].  
227 The adsorbed state gas has the potential becoming free state gas when gas pressure and gas  
228 content decrease and temperature increases [36].

229 Under the isothermal condition, the adsorbed gas volume  $V_m$  is evaluated by Langmuir  
230 isotherm model, given as:

$$V_m = \frac{pV_L}{p + p_L} \quad (2)$$

231 where  $p$  is the equilibrium gas pressure,  $V_L$  and  $p_L$  are the Langmuir Volume and Langmuir  
232 Pressure representing the maximum gas storage capacity and the gas pressure at half Langmuir  
233 Volume, respectively. For the coal samples,  $V_L= 34.98$  mL/g and  $p_L= 1.15$  MPa [28].

234 For intact coal samples, the sizes of pores can be assumed as uniform. Based on this  
235 assumption, a unipore model was developed [37] in order to describe the kinetics of gas  
236 adsorption on coal. The diffusion model can be described as [38]:

$$\frac{V_t}{V_m} = 1 - \frac{6}{\pi^2} \sum_{n=1}^{\infty} \frac{1}{n^2} \exp(-D_e n^2 \pi^2 t) \quad (3)$$

237 where  $V_t$  is the total volume of the diffusing gas that has desorbed at time  $t$ ,  $V_m$  is the total  
238 desorbed gas volume in infinite time, and  $D_e$  is the diffusion coefficient of gas from coal.

239 In particular, for short time ( $< 600$  s) and the desorbed fraction is less than 0.5, the diffusion of  
240 gas in coal  $V_{des}(t)$  can be simplified approximately as below [38, 39]:

$$\frac{V_{des}(t)}{V_m} = \frac{6}{\sqrt{\pi}} \sqrt{D_e t} \quad (4)$$

241 It is well known the statistical duration of outbursts usually in the range of 3~96 s [40]. In  
242 particular, an outburst occurred on 25 April 2009 in Haizi Coal Mine lasted about 10 seconds

243 based on the record of the micro-seismic monitoring system [41]. The gas decompression  
244 process of the present experiments is recorded in Fig. 5. The gas pressure decreases slowly when  
245 the compression test machine starts destressing at first. As the compression test machine running,  
246 the end plates for sealing purpose suddenly separate from the cell, therefore, a sudden drop of  
247 gas pressure occurs. During the sudden drop of gas pressure, the coal briquette initiates  
248 fracturing and even fragmentation. The duration of the drop of gas pressure is about tens of  
249 microseconds. Compared with the decompression process with coal briquettes in the cell  
250 (outburst occurred), no abundant desorbed gas could be detected according to Fig. 5.

251 The so-called outbursts in our experiments occurred within tens of microseconds, here we  
252 suppose the outburst duration is 40 ms. By assuming  $D_e$  to be  $10^{-5} \text{ s}^{-1}$  [38], only about 0.2 %  
253 adsorbed gas can be desorbed during the outburst process from Eq. (3). It is possibly observed  
254 that the outburst initialises when cracks propagate, starts at the fragmentation occurrence, and  
255 finally breaks out as coal fragments ejection with the gas flow. The fracture growth velocity is  
256 rather much faster than the desorption rate. Thus, the fracture is induced by free gas, and the  
257 ejection of coal fragments is contributed by the desorption of gas [23].

### 258 3.6.2 Progressive fragmentation of coal

259 Adsorption in coal is classified as chemical adsorption and physical adsorption. In chemical  
260 adsorption, the adsorbate is bound to the solid surface by a direct chemical bond, and in physical  
261 adsorption, adsorption occurs mainly due to van der Waals and electrostatic forces between the  
262 adsorbate molecules and the atoms composing the adsorbent surface [36]. As a result, coal  
263 swelling results from  $\text{CO}_2$  adsorption. Experimental investigations have been carried out that gas  
264 adsorption can weaken the strength of coal. According to the previous experimental results, the

265 UCS of coal samples decreases with increasing saturated gas and the volumetric strain decreases  
266 as well [42, 43].

267 The gas behaviours (e.g. CH<sub>4</sub>, CO<sub>2</sub>) such as diffusion, emission, adsorption and desorption are  
268 complex processes resulting in physical and chemical behaviours of gas-solid interaction. These  
269 gas behaviours in coal depend on many factors of coal including microstructures, grades, and  
270 water contents. Initially, the inside and outside gas of coal briquettes are at equilibrium when the  
271 coal is saturated in gas, see Fig. 6(a). Suddenly, the rapid decompression of CO<sub>2</sub> takes place.  
272 Since the permeability of coal is not high enough to let the internal free gas of coal flow  
273 promptly. The internal free gas of coal has a potential expansion power which can split the coal  
274 matrix near the tips, see Fig. 6(b). The fracture initiation is observed as the initiation of outburst.  
275 The criterion of outburst can be taken as the criterion of fracture initialisation. It should be worth  
276 noting that fragmentation is the result of sufficient fracture growth, see Fig. 6(c). At the moment  
277 of the fragmentation of coal, the residual gas including undissipated free gas and desorbed gas  
278 contributes to the ejection of fragments.

279 Thus, a criterion for the crack initiation in the coal is introduced as [42]:

$$\Delta p_g \geq \frac{K_c}{\sqrt{\pi a}(1 - \sqrt{\rho/a})} \quad (5)$$

280 where  $\Delta p_g$  is the differential pressure between the gas pressures inside and outside the coal  
281 briquette,  $a$  is the half length of the crack,  $K_c$  is the fracture toughness of the coal filled with gas,  
282 and  $\rho$  is the radius of the curvature of the crack tip.

283 From Eq. (5), it can be understood that the crack initiation depends on the crack length, the  
284 fracture toughness of coal, and the geometry of crack. The gas inside the coal briquettes is  
285 dominant in the outburst occurrence, there is no any initiation of fracture without the differential  
286 gas pressure. The differential pressure is essential for the occurrence of outbursts.

287 3.6.3 Energy components during an outburst

288 The progress of the outburst can be further understood according to the analysis of energy  
 289 release during an outburst. The energy components involved in outbursts are the energy  
 290 generated by free gas  $W_f$  and desorbed gas  $W_{de}$  and the dissipated energy  $E_f$  for fracturing and  
 291 fragmentation of the coal.

292 For an adiabatic process, the total expansion energy of the free gas in coal  $W_f$  can be written  
 293 as [44]:

$$W_f = \frac{(p_g + p_0)V_f}{\kappa - 1} \left[ 1 - \left( \frac{p_0}{p_g + p_0} \right)^{\frac{\kappa-1}{\kappa}} \right] \quad (6)$$

294 where  $p_g$  is the differential pressure between internal gas and atmospheric pressure,  $V_f$  is the  
 295 volume of the free gas,  $\kappa$  is the adiabatic coefficient of CO<sub>2</sub>, 1.30, and  $p_0$  is the atmospheric  
 296 pressure, 0.1 MPa.

297 Given that the adsorbed gas in coal, replace the volume of free gas with the volume of  
 298 adsorbed gas volume from Eq. (1), then the total expansion energy of the adsorbed gas in coal  
 299  $W_{ad}$  is:

$$W_{ad} = \frac{(p_g + p_0)^2 V_L}{(\kappa - 1)(p_g + p_0 + p_L)} \left[ 1 - \left( \frac{p_0}{p_g + p_0} \right)^{\frac{\kappa-1}{\kappa}} \right] \quad (7)$$

300 However, only a portion of the adsorbed gas is involved in the progress of outbursts since the  
 301 duration of the present experimental outburst is tens of microseconds,  $t_0$ . The desorbed gas takes  
 302 part in outbursts can be given by:

$$W_{de} = \frac{6}{\sqrt{\pi}} \sqrt{D_e t_0} \frac{(p_g + p_0)^2 V_L}{(\kappa - 1)(p_g + p_0 + p_L)} \left[ 1 - \left( \frac{p_0}{p_g + p_0} \right)^{\frac{\kappa-1}{\kappa}} \right] \quad (8)$$

303 In general, fragmentation occurs along with outbursts, the energy is from the gas because there  
304 is no other loading applied on the coal briquette. It is worth noting that the more energy  
305 dissipated in the fracturing process, the higher fragmentation degree occurs. We consider a  
306 simple model to evaluate the relationship between the energy dissipated for fracturing and the  
307 fragmentation degree. Then, assumptions are made that the energy acting on fracturing is  
308 proportional to the fracture area at a ratio of the specific surface energy and the all energies from  
309 free gas and desorbed gas can act on fracturing. The shape of fragments is taken as spherical  
310 particles with a mean diameter of  $d$ . The total volume of the coal briquette  $V_{coal}$ . Then the area  
311 of the fracture surface is:

$$A_f = \frac{6}{d}V_{coal} \quad (9)$$

312 Thus, the total energy dissipated by the fragmentation  $E_f$  can be:

$$E_f = \gamma A_f \quad (10)$$

313 where  $\gamma$  is the specific surface energy of the coal. Since the UCS and tensile strength of the coal  
314 briquettes are very low, the specific surface energy is assumed to be  $10^{-4}$  J/m<sup>2</sup> [45].

315 Based on the above analysis, the energy components involved in the experimental outbursts  
316 can be calculated and the results are shown in Fig. 7. For the calculation, the porosity of the coal  
317 briquette is assumed to be 0.15 based on the water content. As gas pressure increases in the coal,  
318 the energy release of free gas and desorbed gas participated in the outburst increase. The  
319 saturated gas pressure of 0.2 MPa in the coal briquette contains the energies of free gas of  
320  $2.3 \times 10^{-6}$  J and desorbed gas of  $2.6 \times 10^{-7}$  J during outbursts. Those energies can only result in **no**  
321 **smaller than** 20 mm of the mean diameter of fragments. As the gas pressure increases to 0.4 MPa,  
322 the free gas and desorbed gas energies become  $5.2 \times 10^{-6}$  J and  $4.1 \times 10^{-7}$  J. A mean diameter of  
323 about **at least** 7 mm of fragmentation can occur. When the saturated gas pressure is 0.6 MPa,

324 more energies released from free gas and desorbed gas can lead to more violent fragmentation.  
325 The energy release of free gas is much larger than the energy release of adsorbed gas. The free  
326 gas is highly possible the main energy for the outburst, but no sufficient evidence can indicate  
327 how much of the free gas and adsorbed gas contribute to the outburst. Valliappan and Wohua [23]  
328 calculated the energy components during outbursts and found the energy releases of free gas and  
329 desorbed gas were larger than the energy dissipation of fragmentation. It also can be observed  
330 that the energy dissipation of the fragmentation and outburst required increases as the intensity  
331 increases. Only slight fragmentation and outburst occurs if the energy release of free gas and  
332 adsorbed gas of the outburst is not sufficient enough.

#### 333 **4 Conclusions**

334 We have performed experiments to investigate the effects of internal gas in coal on outbursts.  
335 So-called outbursts were observed clearly in the experiments, which demonstrated the gas cause.  
336 Based on the experiments, the progress of outburst and the roles of water content, decompression  
337 rate as well as energy components during outbursts were examined. The main findings are  
338 concluded as follows:

339 (1) Coal briquettes of high quality and CO<sub>2</sub> gas were experimented using a designed apparatus to  
340 investigate the mechanism of outburst. The coal briquettes were validated to be practicable  
341 for outbursts. Evident outbursts were observed due to the gas decompression. Critical  
342 minimum gas pressure exists for the outburst occurrence, more violent outbursts can occur as  
343 gas pressure increases.

344 (2) The water content of coal briquettes can significantly affect the initiation of outbursts. For  
345 coal briquettes have higher water content, more water can occupy the micropores of coal,  
346 which can reduce the gas content and coal brittleness, and increase the coal fracture



347 roughness. The expansion energy releases from the gas may not be enough to cause the  
348 fragmentation of coal briquettes when they have higher water content. So, only fractures  
349 appear in the coal briquettes with higher water content. However, violent outbursts can occur  
350 in the coal briquettes with lower water content at the same saturated gas pressure and rate of  
351 gas decompression.

352 (3) The rate of gas decompression is a second key factor to cause the outburst of coal briquettes.  
353 If the rate of gas decompression is lower than the critical minimum rate, the internal gas can  
354 flow and seep out as the coal briquette is an intrinsic porous material. The coal briquettes can  
355 only degas safely if the rate of gas decompression is below the threshold. The rate of gas  
356 decompression corresponds to the gas desorption and gas emission in the coal briquettes. The  
357 coal briquettes can occur fragmentation and outburst if the rate of gas decompression is  
358 above the threshold. The threshold value increases as the water content increases. Further  
359 studies will be conducted to figure the threshold function with the water content in the coal  
360 briquette, which will be presented in the future publications.

361 (4) The evolution of outbursts was identified and discussed. An outburst is the consequence of  
362 the coal fracture and fragmentation mainly caused by the internal gas. Energy components,  
363 i.e. energy release of free gas, desorbed gas, and energy dissipation of fragmentation, were  
364 quantitatively analysed for the experimental outbursts. Free gas possibly contributes mainly  
365 to the outbursts in the experiments, which can be useful to the actual outbursts in coal mining.

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