

# Dynamic-Stress-Induced Enhanced Degradation of $1/f$ Noise in n-MOSFET's

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**Abstract**—AC-stress-induced degradation of  $1/f$  noise is investigated for n-MOSFET's with thermal oxide or nitrided oxide as gate dielectric, and the physical mechanisms involved are analyzed. It is found that the degradation of  $1/f$  noise under ac stress is far more serious than that under dc stress. For an ac stress of  $V_G = 0 \sim 0.5 V_D$ , generations of both interface states ( $\Delta D_{it}$ ) and neutral electron traps ( $\Delta N_{et}$ ) are responsible for the increase of  $1/f$  noise, with the former being dominant. For another ac stress of  $V_G = 0 \sim V_D$ , a large increase of  $1/f$  noise is observed for the thermal-oxide device, and is attributed to enhanced  $\Delta N_{et}$  and generation of another specie of electron traps, plus a small amount of  $\Delta D_{it}$ . Moreover, under the two types of ac stress conditions, much smaller degradation of  $1/f$  noise is observed for the nitrided device due to considerably improved oxide/Si interface and near-interface oxide qualities associated with interfacial nitrogen incorporation.

**Index Terms**— $1/f$  noise, AC hot-carrier stress, dynamic stress, MOSFET's, nitridation.

## I. INTRODUCTION

THE  $1/f$  noise characteristics of MOSFET's are very important because the capability of integrating low-noise analog circuits and high-speed digital circuits on the same chip is crucial to the production of a wide range of high-performance MOS integrated circuits. Therefore, extensive study on degradation of  $1/f$  noise under various kinds of hot-carrier stresses has been made [1]–[3] and different degradations of  $1/f$  noise for different hot-carrier stresses were found [4], [5]. However, to our knowledge, these experimental studies concerned only dc hot-carrier stresses, while MOSFET's in real circuits are exposed to transient gate-and drain-voltage conditions. It is therefore more meaningful to investigate ac hot-carrier-induced degradation of  $1/f$  noise. In this work, two typical ac stress conditions with  $V_G$  pulsed between 0 and  $0.5 V_D$  or 0 and  $V_D$  are used to investigate the degradation behaviors of  $1/f$  noise for n-MOSFET's with thermal oxide or nitrided oxide as gate dielectric. Frequency-and duty-cycle-dependent degradations of  $1/f$  noise are also examined and the physical mechanisms involved are discussed. It is observed that, although the ac hot-carrier stresses induce a larger noise degradation than dc

hot-carrier stresses for thermal-oxide device, significantly improved  $1/f$  noise properties are obtained for nitrided devices.

## II. EXPERIMENTS

The n-channel MOSFET's used in this study were fabricated on p-type (100) silicon wafers with a resistivity of 6–8  $\Omega$ -cm by a self-aligned n<sup>+</sup> polysilicon gate process. After the channel region was implanted by B<sup>+</sup> through a sacrificial oxide which was then stripped, thermal gate oxide (OX) was grown at 850 °C for 70 min in dry O<sub>2</sub>. N<sub>2</sub>O-nitrided oxide (N<sub>2</sub>ON) was obtained by annealing a thinner thermal oxide (grown at 850 °C for 60 min in dry O<sub>2</sub>) at 950 °C for 20 min in pure N<sub>2</sub>O ambient so as to achieve the same thickness. The two gate oxides were finally annealed in N<sub>2</sub> at 950 °C for 25 min. Final thickness measured by capacitance–voltage technique was about 160 Å for both oxides. Aluminum was thermally evaporated, and then patterned, followed by a forming gas anneal at 410 °C for 30 min. Two ac hot-carrier stresses (gate voltage  $V_G$  pulsed between  $V_{Gi} = 0$  V and  $V_{Gh} = 4$  or 8 V, a fixed drain voltage  $V_D = 8$  V, source and substrate grounded) were, respectively, applied on n-MOSFET's with channel width  $W$ /length  $L$  of 20  $\mu$ m/2  $\mu$ m and 10  $\mu$ m/3  $\mu$ m to investigate the degradation behaviors of  $1/f$  noise. Since experimental data of the latter were similar to that of the former, only the results of the former were reported below. A unipolar square waveform was supplied by HP41501A pulse generator expander with built-in filter function, which suppressed possible voltage overshoot (the maximum value was 230 mV when  $V_{Gh} = 8$  V and  $f = 100$  kHz). The  $1/f$  noise was measured at 50 Hz using HP 35665A dynamic signal analyzer, BTA 9603 FET noise analyzer, and HP 4145B semiconductor parameter analyzer in the linear region of device operation ( $V_D = 0.2$  V) for a gate overdrive voltage  $V_G^* = V_G - V_T = 0.5$  V ( $V_T$  is the threshold voltage). Moreover, a charge-pumping (CP) technique, which varied pulse base level to drive the silicon surface from accumulation to inversion while keeping the amplitude of the pulse constant ( $\Delta V_G = 5$  V) with reverse-biased source and drain (0.1 V), was also used to obtain information on interface-state density.

## III. RESULTS AND DISCUSSION

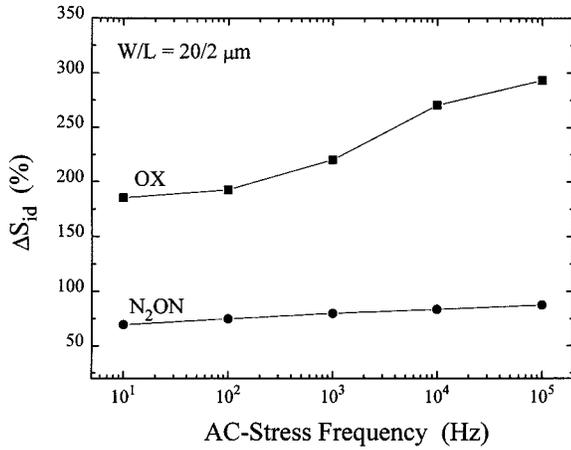
The  $1/f$  noise is characterized by the noise power ( $S_{id}$ ) of drain current which is derived from a unified  $1/f$  noise model incorporating both number fluctuation and surface mobility fluctuation [6]. Fig. 1(a) shows the percentage  $S_{id}$  degradation ( $\Delta S_{id}$ ) for n-MOSFET's after a 3000-s ac stress at  $V_D = 8$  V,  $V_G$  pulsed between  $V_{Gi} = 0$  V and  $V_{Gh} = 4$  V with

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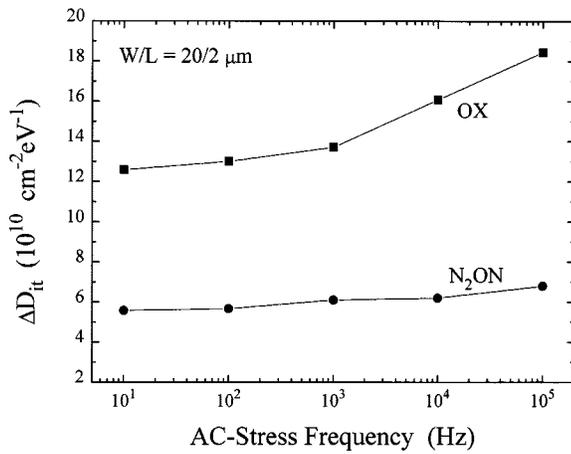
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(a)



(b)

Fig. 1. Frequency dependence of (a)  $1/f$  noise degradation and (b) interface-state generation after a 3000-s ac stress with  $V_D = 8$  V and  $V_G$  pulsed between  $V_{Gi} = 0$  V and  $V_{Gh} = 4$  V. Rise/fall times of the gate pulse are 200 ns with 50% duty cycle. Noise measurement conditions are  $f = 50$  Hz,  $V_D = 0.2$  V and  $V_G^* = 0.5$  V. The corresponding dc stress-induced  $S_{id}/D_{it}$  degradations at  $V_D = 2V_G = 8$  V are 181%/11.4  $\times 10^{10}$  cm<sup>-2</sup> eV<sup>-1</sup> for OX sample and 65%/5.4  $\times 10^{10}$  cm<sup>-2</sup> eV<sup>-1</sup> for N<sub>2</sub>ON sample.

rise/fall times of 200 ns and 50% duty cycle. The corresponding dc-stress-induced degradations at  $V_D = 2V_G = 8$  V, which is mainly associated with interface-state generation under maximum substrate current [7], are 181% for OX sample and 65% for N<sub>2</sub>ON sample. It can be seen that ac stress-induced  $\Delta S_{id}$  increases with frequency and is larger than dc stress-induced  $\Delta S_{id}$ , especially for  $f > 10^3$  Hz. Similar frequency dependence of increased interface-state density measured by CP technique is also observed, as shown in Fig. 1(b). This is consistent with the results in [8]. As a result,  $\Delta D_{it}$  should be mainly responsible for  $\Delta S_{id}$ , while other factors should be hole trapping and generation of neutral electron traps near the interface due to the presence of the low- $V_G$  half cycle during the ac stress with  $V_D$  fixed at high voltage [9], [10]. This is supported by the larger value of  $\Delta S_{id}$  than that of  $\Delta D_{it}$  measured at  $f = 10^4$  Hz, as shown in Fig. 2. Furthermore, the drain-current noise power spectrum of OX sample is measured before and after a 3000-s ac stress at  $f = 10^4$  Hz under the same conditions as in Fig. 1. As can be seen from Fig. 3, the measured low-frequency noise is indeed a  $1/f$  noise with a

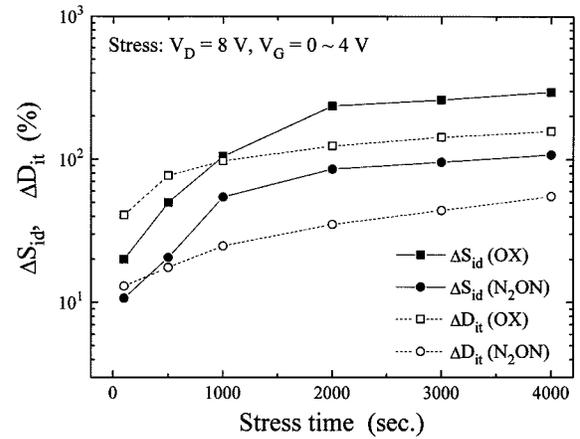


Fig. 2. Degradation of  $1/f$  noise as a function of stress time under the same ac stress voltage conditions as that in Fig. 1 at a frequency of  $10^4$  Hz with 50% duty cycle. Noise measurement conditions are same as that in Fig. 1.

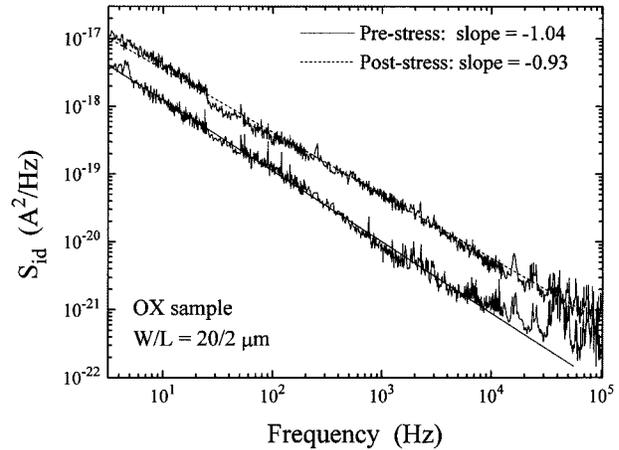


Fig. 3. Drain-current noise power spectrum of OX sample before and after a 3000-s ac stress at  $f = 10^4$  Hz under the same conditions as Fig. 1. The error of extracted slope values is  $\pm 0.003$ .

slope of  $-1.04$  (prestress) or  $-0.93$  (post-stress). A reduction of the slope after the stress implies a nonuniform generation of interface and near-interface traps, i.e., generation of high-frequency traps (traps close to the interface) is more than that of low-frequency traps (traps away from the interface). Therefore, a larger degradation of  $1/f$  noise occurs at the high-frequency end than at the low-frequency end. In addition, it is worth pointing out that in the initial stage of the ac stress in Fig. 2,  $\Delta S_{id}$  is even smaller than  $\Delta D_{it}$ . This is probably because most initially created interface states lies at the interface (fast interface states) so that fluctuation in the number of channel carriers due to tunneling between the interface states and the inversion layer is too quick to be detected in the typical frequency range of noise measurements [11]. Moreover,  $\Delta N_{et}$  is also small in the initial stage. For longer stress time, besides a large  $\Delta D_{it}$  including both fast interface states and near-interface oxide traps (the two are indistinguishable in CP measurement, but the latter can be detected by noise measurement [11]), hole trapping and generation of neutral electron traps become also serious, thus resulting in  $\Delta S_{id}$  larger than  $\Delta D_{it}$ . Compared to OX sample, N<sub>2</sub>ON sample exhibits greatly suppressed  $\Delta S_{id}$  due to hardened oxide/Si interface and near-interface oxide

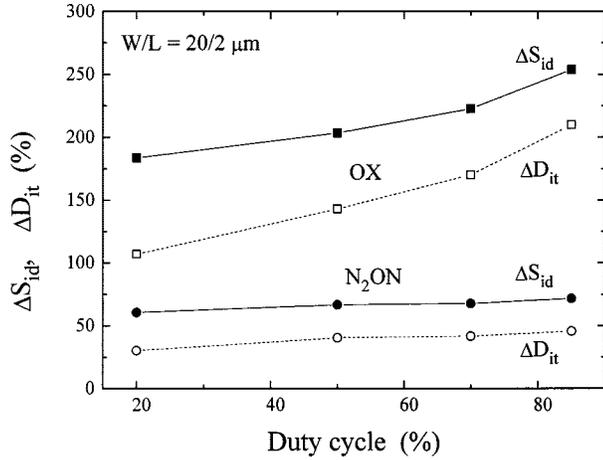


Fig. 4. Duty-cycle dependence of  $1/f$  noise degradation under an ac stress with  $V_D = 8$  V and  $V_G$  pulsed between  $V_{Gi} = 0$  V and  $V_{Gh} = 4$  V at a frequency of  $10^4$  Hz. Rise/fall times of the gate pulse are 200 ns. Noise measurement conditions are same as that in Fig. 1.

resulting from  $N_2O$  nitridation and thus smaller  $\Delta D_{it}$  and  $\Delta N_{et}$ . Based on the above discussion, it can be concluded that  $\Delta S_{id}$  induced by ac stress at  $V_G = 0-4$  V and  $V_D = 8$  V is a combined effect of  $\Delta D_{it}$  and  $\Delta N_{et}$ .

To further clarify the impacts of  $\Delta D_{it}$  and  $\Delta N_{et}$  on  $\Delta S_{id}$ , duty-cycle dependence of  $1/f$  noise degradation is examined under an ac stress for 2000 s at  $V_D = 8$  V and  $V_G = 0-4$  V with  $f = 10^4$  Hz and rise/fall times of 200 ns, and the results are depicted in Fig. 4. For OX sample,  $\Delta S_{id}$  increases significantly with duty cycle, while a weak dependence of  $\Delta S_{id}$  on duty cycle is found for  $N_2ON$  sample. As mentioned above, there is neutral electron-trap generation in the low- $V_G$  portion of a cycle and interface-state generation in the high- $V_G$  portion of a cycle. So, for larger duty cycle, the stress condition of  $V_D = 2V_G = 8$  V occurs for a larger fraction of the total ac stress duration, yielding larger  $\Delta D_{it}$ , while  $\Delta N_{et}$  dominates for small duty cycles. This fact is well illustrated by the gradual closeness of  $\Delta D_{it}$  to  $\Delta S_{id}$  at larger duty cycles. However,  $\Delta D_{it}$  of  $N_2ON$  sample is hardly sensitive to duty cycle due to considerably enhanced interface hardness against hot-carrier bombardment, and thus a weak duty-cycle dependence of  $\Delta S_{id}$  results. In view of the above analysis and further comparing the  $\Delta S_{id}$  values at the two ends of duty cycle, it can be believed that  $\Delta S_{id}$  is influenced to a larger extent by  $\Delta D_{it}$  than  $\Delta N_{et}$ , at least for duty cycles  $\geq 50\%$ .

Presented in Fig. 5 is another ac stress-induced degradation of  $S_{id}$  when  $V_G$  is pulsed between a wider range (0–8 V) with other conditions same as those in Fig. 2. Surprisingly, in the whole stress duration, a larger  $\Delta S_{id}$  of OX sample is induced by the ac stress as compared to the stress in Fig. 2, while the opposite holds for  $N_2ON$  sample, with both devices displaying smaller  $\Delta D_{it}$ . This can be explained as followings. Like the previous ac stress, in the low- $V_G$  half cycle, there are hole trapping and  $\Delta N_{et}$ . Since  $N_{et}$  is believed to be created through the recombination of injected electrons and trapped holes [12], an enhanced  $\Delta N_{et}$  should result due to  $V_{Gh} = V_D = 8$  V in this ac stress, which can lead to a large amount of electron injection [7]. Moreover, under this ac stress, another specie of electron traps can also be created by the injected hot electrons, with its

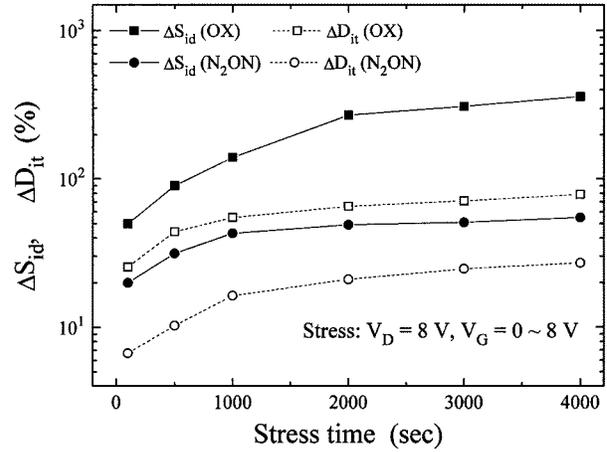


Fig. 5. Degradation of  $1/f$  noise as a function of stress time under an ac stress with  $V_D = 8$  V and  $V_G$  pulsed between  $V_{Gi} = 0$  V and  $V_{Gh} = 8$  V at a frequency of  $10^4$  Hz. Rise/fall times of the gate pulse are 200 ns with 50% duty cycle. Noise measurement conditions are same as that in Fig. 1.

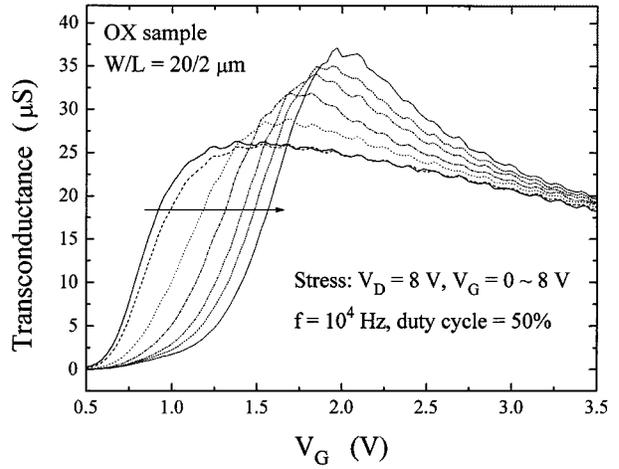


Fig. 6. Transconductance characteristics of OX device under the ac stress conditions in Fig. 4. Along the arrow direction, stress time is 0, 100, 500, 1000, 2000, 3000, and 4000 s.

physical or microscopic nature different from the one created by hot holes at low gate voltage [13]. All these happen in the gate oxide close to the oxide/Si interface near the drain. So, a damaged region near the drain is easily formed when all these electron trap generation/trapping are serious. This is true for OX sample as demonstrated by its transconductance behaviors in Fig. 6, because its peak linear transconductance  $G_m$  increases and the curve shifts to higher  $V_G$  (implying higher  $V_T$ ) as the ac stress progresses. This is just an indication of gradual formation of a damaged region near the drain [14]. Therefore, it can be deduced that a large amount of generated electron traps along with  $\Delta D_{it}$  cause a large carrier-number fluctuation and thus a large  $\Delta S_{id}$  under the ac stress of  $V_D = 8$  V and  $V_G = 0-8$  V. However, for  $N_2ON$  sample, owing to nitrogen incorporation near its oxide/Si interface which introduces stronger Si–N bonds ( $E_{Si-N} \sim 4.6$  eV) [15], [16] and relaxes interfacial strained Si–O bonds [17], the two kinds of electron-trap generations and  $\Delta D_{it}$  are considerably suppressed and no damaged region is formed near the drain, thus resulting in a much smaller  $\Delta S_{id}$  as observed in Fig. 5.

## IV. SUMMARY

Degradation behaviors of  $1/f$  noise under dynamic stress are investigated for n-MOSFET's with nitrided oxide or thermal oxide as gate dielectric. Compared to static stress, dynamic stress results in a larger increase of  $1/f$  noise. This is because not only interface states but also electron traps are created during dynamic stress. However, nitrided devices show significantly improved immunity to dynamic stress-induced degradation in  $1/f$  noise due to nitrogen incorporation near the oxide/Si interface which hardens the interface and near-interface oxide, and thus suppresses generations of interface states and electron traps.

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